

MAU34405: Statistical Physics I

Homework 2 due 08/11/2021

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Exercise 1

$$\begin{aligned} dE &= \frac{\partial E}{\partial X_1} dX_1 + \frac{\partial E}{\partial X_2} dX_2 \\ &= P_1 dX_1 + P_2 dX_2 \\ \implies P_i &= \frac{\partial E}{\partial X_i}, \quad i = 1, 2 \end{aligned}$$

$$\begin{aligned} \text{Consider } d\Phi_i &\equiv d(E - P_i X_i) \\ &= P_1 dX_1 + P_2 dX_2 - X_i dP_i - P_i dX_i \\ &= -X_i dP_i + P_j dX_j, \quad i, j = 1, 2, i \neq j \\ \implies \Phi_i &= \Phi_i(P_i, X_j) \end{aligned}$$

$$\begin{aligned} \frac{\partial^2 \Phi_i}{\partial P_i^2} &= \frac{\partial(-X_i)}{\partial P_i} & \frac{\partial^2 \Phi_i}{\partial X_j^2} &= \frac{\partial P_j}{\partial X_j} \\ &= -\left(\frac{\partial P_i}{\partial X_i}\right)^{-1} & &= \frac{\partial^2 E}{\partial X_j^2} \\ &= -\left(\frac{\partial^2 E}{\partial X_i^2}\right)^{-1} & \geq 0 &\implies \Phi_i \text{ convex function of } X_j \\ &\leq 0 \implies \Phi_i \text{ concave function of } P_i \end{aligned}$$

$$\begin{aligned} \text{Consider } d\Psi &\equiv d(E - P_1 X_1 - P_2 X_2) \\ &= P_1 dX_1 + P_2 dX_2 - X_1 dP_1 - P_1 dX_1 - X_2 dP_2 - P_2 dX_2 \\ &= -X_1 dP_1 - X_2 dP_2 \\ \implies \Psi &= \Psi(P_1, P_2) \end{aligned}$$

$$\begin{aligned} \frac{\partial^2 \Psi}{\partial P_i^2} &= \frac{\partial(-X_i)}{\partial P_i} \\ &= -\left(\frac{\partial P_i}{\partial X_i}\right)^{-1} \\ &= -\left(\frac{\partial^2 E}{\partial X_i^2}\right)^{-1} \\ &\leq 0 \end{aligned}$$

$$\begin{aligned} \frac{\partial^2 \Psi}{\partial P_1^2} \frac{\partial^2 \Psi}{\partial P_2^2} - \left(\frac{\partial^2 \Psi}{\partial P_1 \partial P_2}\right)^2 &= \frac{\partial(-X_1)}{\partial P_1} \frac{\partial(-X_2)}{\partial P_2} - \left(\frac{\partial(-X_2)}{\partial P_1}\right)^2 \\ &= \left(\frac{\partial P_1}{\partial X_1} \frac{\partial P_2}{\partial X_2}\right)^{-1} - \left(\frac{\partial P_1}{\partial X_2}\right)^{-2} \\ &= \left(\frac{\partial^2 E}{\partial X_1^2} \frac{\partial^2 E}{\partial X_2^2}\right)^{-1} - \left(\frac{\partial^2 E}{\partial X_2 \partial X_1}\right)^{-2} \\ \frac{\partial^2 E}{\partial X_1^2} \frac{\partial^2 E}{\partial X_2^2} - \left(\frac{\partial^2 E}{\partial X_2 \partial X_1}\right)^2 &\geq 0 \implies \left(\frac{\partial^2 E}{\partial X_1^2} \frac{\partial^2 E}{\partial X_2^2}\right)^{-1} - \left(\frac{\partial^2 E}{\partial X_2 \partial X_1}\right)^{-2} \leq 0 \\ \implies \frac{\partial^2 \Psi}{\partial P_1^2} \frac{\partial^2 \Psi}{\partial P_2^2} - \left(\frac{\partial^2 \Psi}{\partial P_1 \partial P_2}\right)^2 &\leq 0 \end{aligned}$$

Thus any Legendre transform of E , whether it has one or two intensive variables, will be a convex function of its extensive variables and a concave function of its intensive parameters.

Exercise 2

1.

First: derive the adiabatic process equations.

$$\begin{aligned}
 \text{Ideal gas, reversible process} &\implies C_V \equiv \left(\frac{\partial E}{\partial T} \right)_V = \frac{dE}{dT} \\
 &\implies dE = C_V dT \\
 dQ &= dE - dW \\
 &= C_V dT + P dV \\
 C_P &\equiv \frac{dQ_P}{dT} \\
 &= \left(\frac{\partial}{\partial T} \right)_P dQ \\
 &= C_V + P \left(\frac{\partial V}{\partial T} \right)_P
 \end{aligned}$$

$$\begin{aligned}
 PV &= kNT \\
 \implies \left(\frac{\partial}{\partial T} \right)_P (PV) &= \left(\frac{\partial}{\partial T} \right)_P (kNT) \\
 \implies P \left(\frac{\partial V}{\partial T} \right)_P &= kN \\
 \implies C_P &= C_V + kN \\
 \implies \frac{kN}{C_V} &= \gamma - 1, \quad \gamma \equiv \frac{C_P}{C_V}
 \end{aligned}$$

$$\begin{aligned}
 \text{Adiabatic} &\implies 0 = dQ \\
 &= dE + P dV \\
 &= C_V dT + \frac{kNT}{V} dV \\
 \implies C_V \frac{dT}{T} &= C_V (1 - \gamma) \frac{dV}{V} \\
 \implies \ln T &= (1 - \gamma) \ln V + \alpha \\
 \implies T &= e^\alpha V^{1-\gamma} \\
 \implies TV^{\gamma-1} &= e^\alpha
 \end{aligned}$$

$$\begin{aligned}
 T = \frac{PV}{kN} &\implies \frac{PV}{kN} V^{\gamma-1} = e^\alpha & V = \frac{kNT}{P} &\implies T \left(\frac{kNT}{P} \right)^{\gamma-1} = e^\alpha \\
 &\implies PV^\gamma = kN e^\alpha & &\implies T^\gamma P^{1-\gamma} = \frac{e^\alpha}{(kN)^{\gamma-1}} \\
 & & &\implies PT^{\frac{\gamma}{1-\gamma}} = \left(\frac{e^\alpha}{(kN)^{\gamma-1}} \right)^{\frac{1}{1-\gamma}}
 \end{aligned}$$

$$e, \alpha, k, N, \gamma \text{ constants} \implies PV^\gamma = \text{constant} \quad TV^{\gamma-1} = \text{constant} \quad PT^{\frac{\gamma}{1-\gamma}} = \text{constant}$$

As is clear from the figure, the system attains its minimum volume V_1 at point B , its maximum volume V_2 at points A and D , its minimum pressure P_1 at point A , and its maximum pressure P_2 at points B and C .

From investigating the figure, we can see that $V_B < V_C$ and $P_B = P_C$, and $V_A = V_D$ and $P_A < P_D$. From $PV = kNT$, we can deduce that the minimum temperature T_1 must occur at either A or B , and the maximum temperature T_2 at C or D .

$$\begin{aligned} T_A V_A^{\gamma-1} &= T_B V_B^{\gamma-1} & T_C V_C^{\gamma-1} &= T_D V_D^{\gamma-1} \\ T_A V_2^{\gamma-1} &= T_B V_1^{\gamma-1} & T_C V_C^{\gamma-1} &= T_D V_2^{\gamma-1} \\ \frac{T_A}{T_B} &= \left(\frac{V_1}{V_2}\right)^{\gamma-1} & \frac{T_C}{T_D} &= \left(\frac{V_2}{V_C}\right)^{\gamma-1} \\ V_1 < V_2 &\implies T_A < T_B & V_2 > V_C &\implies T_C > T_D \\ &\implies T_A = T_1 & & T_C = T_2 \end{aligned}$$

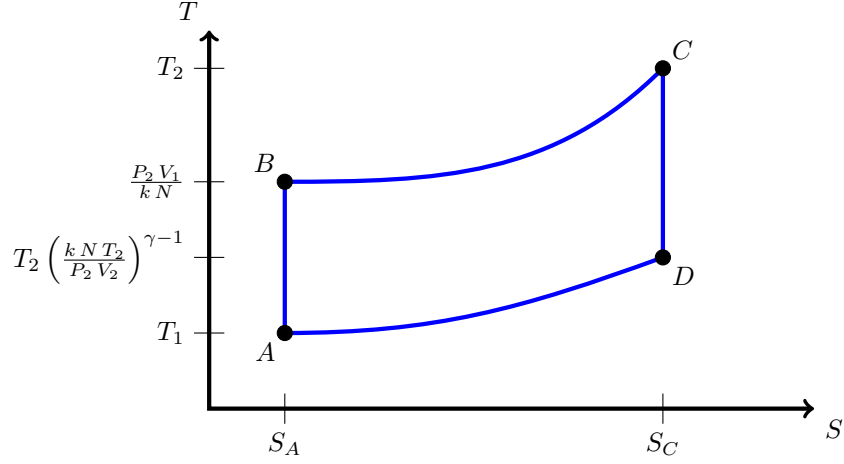
$$\begin{aligned} P_B V_B &= kNT_B & P_C V_C &= kNT_C \\ P_2 V_1 &= kNT_B & P_2 V_C &= kNT_2 \\ T_B &= \frac{P_2 V_1}{kN} & V_C &= \frac{kNT_2}{P_2} \end{aligned}$$

$$\begin{aligned} P_C V_C^\gamma &= P_D V_D^\gamma & T_C V_C^{\gamma-1} &= T_D V_D^{\gamma-1} \\ P_2 \left(\frac{kNT_2}{P_2}\right)^\gamma &= P_D V_2^\gamma & T_2 \left(\frac{kNT_2}{P_2}\right)^{\gamma-1} &= T_D V_2^{\gamma-1} \\ P_D &= P_2 \left(\frac{kNT_2}{P_2 V_2}\right)^\gamma & T_D &= T_2 \left(\frac{kNT_2}{P_2 V_2}\right)^{\gamma-1} \end{aligned}$$

$$\begin{aligned} (P_A, V_A, T_A) &= (P_1, V_2, T_1) & (P_C, V_C, T_C) &= \left(P_2, \frac{kNT_2}{P_2}, T_2\right) \\ (P_B, V_B, T_B) &= \left(P_2, V_1, \frac{P_2 V_1}{kN}\right) & (P_D, V_D, T_D) &= \left(P_2 \left(\frac{kNT_2}{P_2 V_2}\right)^\gamma, V_2, T_2 \left(\frac{kNT_2}{P_2 V_2}\right)^{\gamma-1}\right) \end{aligned}$$

2.

$$\begin{aligned} S &= ckN \ln\left(\frac{E}{E_0}\right) + kN \ln\left(\frac{V}{V_0}\right) + f(N) \\ E = ckNT, N \text{ constant} &\implies \Delta S_{i \rightarrow f} = S_f - S_i = ckN \ln\left(\frac{T_f}{T_i}\right) + kN \ln\left(\frac{V_f}{V_i}\right) \\ A \rightarrow B : T_B > T_A, \text{ adiabatic} &\implies \Delta S_{A \rightarrow B} = 0 \\ B \rightarrow C : T_C > T_B, V_C > V_B &\implies \Delta S_{B \rightarrow C} = ckN \ln\left(\frac{T_C}{T_B}\right) + kN \ln\left(\frac{V_C}{V_B}\right) > 0 \\ C \rightarrow D : T_D < T_C, \text{ adiabatic} &\implies \Delta S_{C \rightarrow D} = 0 \\ D \rightarrow A : T_A < T_D, V_A = V_D &\implies \Delta S_{D \rightarrow A} = ckN \ln\left(\frac{T_A}{T_D}\right) < 0 \end{aligned}$$



3.

$$\eta = \frac{W}{Q_{\text{abs}}} = \frac{Q_{\text{abs}} - Q_{\text{exp}}}{Q_{\text{abs}}} = 1 - \frac{Q_{\text{exp}}}{Q_{\text{abs}}}$$

We only need to calculate the heat transfer during $B \rightarrow C$ and $D \rightarrow A$, since $A \rightarrow B$ and $C \rightarrow D$ are adiabatic and thus have no heat transfer.

$$\begin{aligned} Q_{\text{abs}} &= dQ_{B \rightarrow C} \\ &= \Delta E_{B \rightarrow C} + dW_{B \rightarrow C} \\ &= c k N (T_C - T_B) - \int_{V_B}^{V_C} P dV \\ &= c k N \left(T_2 - \frac{P_2 V_1}{k N} \right) - P_2 \left(\frac{k N T_2}{P_2} - V_1 \right) \\ &= (c - 1) (k N T_2 - P_2 V_1) \end{aligned} \quad \begin{aligned} -Q_{\text{exp}} &= dQ_{D \rightarrow A} \\ &= \Delta E_{D \rightarrow A} + dW_{D \rightarrow A} \\ &= c k N (T_A - T_D) - \int_{V_D}^{V_A} P dV \\ &= c k N \left(T_1 - T_2 \left(\frac{k N T_2}{P_2 V_2} \right)^{\gamma-1} \right) - 0 \\ &= c k N \left(T_1 - T_2 \left(\frac{k N T_2}{P_2 V_2} \right)^{\gamma-1} \right) \end{aligned}$$

$$\Rightarrow \eta = 1 + \frac{c k N}{(c - 1) (k N T_2 - P_2 V_1)} \left(T_1 - T_2 \left(\frac{k N T_2}{P_2 V_2} \right)^{\gamma-1} \right)$$

Exercise 3

$$\begin{aligned}\left.\frac{dP}{dT}\right|_{\text{boundary}} &= \frac{L}{T \Delta v} \\ &= \frac{L}{T \left(\frac{V_v}{N_v} - \frac{V_l}{N_l} \right)} \\ &= \frac{L}{T \frac{V_v}{N_v}}\end{aligned}$$

(neglecting the volume of the liquid compared to that of the vapor, i.e. $\frac{V_v}{N_v} \gg \frac{V_l}{N_l}$)

$$\begin{aligned}&= \frac{P L}{k T^2} & (P = \frac{k N T}{V} \implies \frac{1}{\frac{V_v}{N_v}} = \frac{P}{k T}) \\ \frac{dP}{P} &= \frac{L}{k} \frac{dT}{T^2} \\ \int_{P_0}^P \frac{dP}{P} &= \frac{L}{k} \int_{T_0}^T \frac{dT}{T^2} \\ \ln \left(\frac{P}{P_0} \right) &= \frac{L}{k} \left(\frac{1}{T_0} - \frac{1}{T} \right) \\ P &= P_0 \exp \left(\frac{L}{k} \left(\frac{1}{T_0} - \frac{1}{T} \right) \right)\end{aligned}$$

Exercise 4

1.

$$\begin{aligned}P &= \frac{k T}{\frac{V}{N} - b} - \frac{a N^2}{V^2} \\ 0 &= \left. \frac{\partial P}{\partial V} \right|_{\text{critical point}} \\ &= -\frac{k T_c}{N \left(\frac{V_c}{N} - b \right)^2} + \frac{2a N^2}{V_c^3} \\ \frac{6a N^2}{V_c^4} &= \frac{3k T_c}{N V_c \left(\frac{V_c}{N} - b \right)^2} \tag{1}\end{aligned}$$

$$\begin{aligned}0 &= \left. \frac{\partial^2 P}{\partial V^2} \right|_{\text{critical point}} \\ &= \frac{2k T_c}{N^2 \left(\frac{V_c}{N} - b \right)^3} - \frac{6a N^2}{V_c^4} \\ (1) \implies \frac{3k T_c}{N V_c \left(\frac{V_c}{N} - b \right)^2} &= \frac{2k T_c}{N^2 \left(\frac{V_c}{N} - b \right)^3} \\ 3N \left(\frac{V_c}{N} - b \right) &= 2V_c \\ V_c &= 3b N\end{aligned}$$

$$\begin{aligned}
(1) \implies \frac{2a N^2}{27b^3 N^3} &= \frac{k T_c}{N (3b - b)^2} \\
T_c &= \frac{4b^2 N}{k} \frac{2a}{27b^3 N} \\
&= \frac{8a}{27kb}
\end{aligned}$$

$$\begin{aligned}
P_c &= \frac{k T_c}{\frac{V_c}{N} - b} - \frac{a N^2}{V_c^2} \\
&= \frac{\frac{8a}{27b}}{3b - b} - \frac{a N^2}{9b^2 N^2} \\
&= \frac{4a}{27b^2} - \frac{a}{9b^2} \\
&= \frac{a}{27b^2}
\end{aligned}$$

$$T_c = \frac{8a}{27kb}$$

$$P_c = \frac{a}{27b^2}$$

$$V_c = 3bN$$

2.

$$\begin{aligned}
G &= E + PV - TS \\
dG &= T dS - P dV + \mu dN + V dP + P dV - S dT - T dS \\
&= -S dT + V dP + \mu dN \\
dP &= \left(\frac{\partial P}{\partial T} \right)_{V,N} dT + \left(\frac{\partial P}{\partial V} \right)_{T,N} dV + \left(\frac{\partial P}{\partial N} \right)_{T,V} dN \\
\implies dG &= \left(V \left(\frac{\partial P}{\partial T} \right)_{V,N} - S \right) dT + V \left(\frac{\partial P}{\partial V} \right)_{T,N} dV + \left(\mu + \left(\frac{\partial P}{\partial N} \right)_{T,V} \right) dN
\end{aligned}$$

$$\begin{aligned}
\left. \frac{\partial G}{\partial V} \right|_{\text{critical point}} &= V \left(\frac{\partial P}{\partial V} \right)_{T,N} \Big|_{\text{critical point}} & \left. \frac{\partial^2 G}{\partial V^2} \right|_{\text{critical point}} &= \frac{\partial}{\partial V} \left(V \left(\frac{\partial P}{\partial V} \right)_{T,N} \right) \Big|_{\text{critical point}} \\
&= V_c \cdot 0 & &= \left(\frac{\partial P}{\partial V} \right)_{T,N} \Big|_{\text{critical point}} + V \left(\frac{\partial^2 P}{\partial V^2} \right)_{T,N} \Big|_{\text{critical point}} \\
\left. \frac{\partial G}{\partial V} \right|_{\text{critical point}} &= 0 & \left. \frac{\partial^2 G}{\partial V^2} \right|_{\text{critical point}} &= 0
\end{aligned}$$

Both first and second derivatives of the Gibbs free energy with respect to volume are zero at the critical point, implying that the critical point is a saddle point when considering G as a function of V at constant temperature. This is as expected, as the derivative on the boundary does not jump between values based on which phase the system is in due to it being at its critical point, i.e. a point at which phases are indistinguishable.