

# Computation Lab - Nonlinear Pendulum

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## Abstract

A computer program was written to model the simple pendulum. Cases of undamped, damped, and damped + driven were considered. In the two non-driven cases, comparisons were drawn between the cases of linear and non-linear modelling by comparing phase diagrams of each system for a series of initial conditions. In the case of the damped, driven pendulum, the effect of a control parameter was explored, namely the amplitude of the driving force. Period-doubling was demonstrated and it was found that for the value  $a=1.5$ , the system became chaotic.

## Aims

To computationally model the following systems:

- a simple pendulum (linear and nonlinear)
- a damped pendulum (linear and nonlinear)
- a damped, driven nonlinear pendulum

## Introduction and Theory

The most general form for describing a pendulum consisting of a bob at the end of a light inextensible string of length  $L$  is as follows:

$$\frac{d^2\theta}{dt^2} = -\beta^2 \sin(\theta) - k\omega = a \cos(\Omega t)$$

In this equation,  $\beta = \sqrt{\frac{g}{L}}$ ,  $k$  is a damping coefficient,  $a$  is the amplitude of the driving force and  $\Omega$  its frequency. This can be specialised to the

undamped or undriven cases by letting  $k = 0$  or  $a = 0$ , respectively. It can be further specialised to the linear case by making the approximation  $\sin(\theta) \approx \theta$ .

## The Simple Euler Method

The *Simple Euler Method* uses Taylor series expansions for  $\theta$  and  $\omega$ , ignoring terms of order 2 or higher:

$$\theta(t + \Delta t) = \theta(t) + \dot{\theta}\Delta t + \dots$$

or, with a slight change in notation

$$\theta_{n+1} = \theta_n + \omega_n \Delta t$$

Similar analysis for  $\omega$  yields:

$$\omega_{n+1} = \omega_n - \theta_n \Delta t$$

However, this is only accurate to first order, and thus not very useful for our particular purposes.

## Trapezoidal Rule

An improvement on the simple Euler method, the trapezoidal rule calculates the area of the trapezoid between  $t$  and  $\Delta t$ :

$$\int_t^{t+\Delta t} \frac{d\theta}{dt} dt = \theta_{n+1} - \theta_n \approx ((t + \Delta t) - t) \frac{\frac{d\theta(t)}{dt} + \frac{d\theta(t+\Delta t)}{dt}}{2}$$

Which, taking a Taylor expansion, gives

$$\theta_{n+1} \approx \theta_n + \frac{k1a + k2a}{2}$$

where

$$k1a = \omega_n \Delta t$$

$$k2a = (\omega_n + f(\theta_n, \omega_n, t) \Delta t) \Delta t$$

Similarly, we find

$$\omega_{n+1} \approx \omega_n + \frac{k1b + k2b}{2}$$

Where

$$k2b = (f(\theta_{n+1}, \omega_n + k1b, t_{n+1})) \Delta t$$

## The Runge-Kutta Method

The fourth order Runge Kutta method is a more accurate approximation given by the following equations:

$$\begin{aligned}k1a &= h\omega \\k2a &= h\left(\frac{\omega + k1b}{2}\right) \\k3a &= h\left(\frac{\omega + k2b}{2}\right) \\k4a &= h(\omega + k3b) \\k1b &= hf(\theta, \omega, t) \\k2b &= hf\left(\theta + \frac{k1a}{2}, \omega + \frac{k1b}{2}, t + \frac{h}{2}\right) \\k3b &= hf\left(\theta + \frac{k2a}{2}, \omega + \frac{k2b}{2}, t + \frac{h}{2}\right) \\k4b &= hf(\theta + k3a, \omega + k3b, t + h) \\\theta(t + h) &= \theta(t) + \frac{(k1a + 2k2a + 2k3a + k4a)}{6} \\\omega(t + h) &= \omega(t) + \frac{(k1b + 2k2b + 2k3b + k4b)}{6}\end{aligned}$$

## Experimental Method

Firstly, a C-program utilising the trapezoidal rule was used to create sets of data for both undamped and damped pendula in both the linear and non-linear case, for initial starting angles of 0.2, 1 and 3.124. Using Gnuplot, time-dependence graphs of angle and angular velocity were plotted, along with phase diagrams for each initial angle.

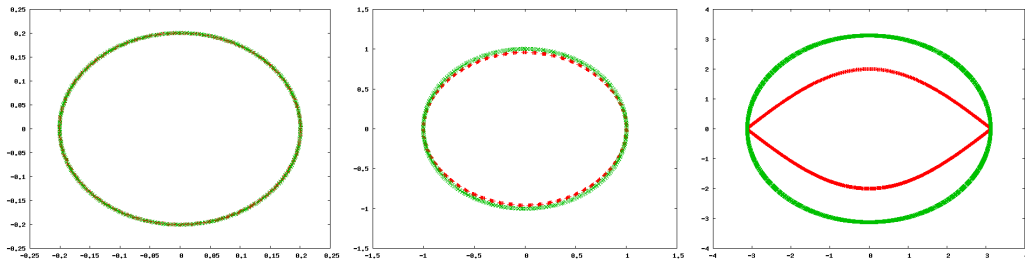
Next, using a modified C-program utilising the Runge-Kutta method, data was attained for the case of the damped, driven non-linear pendulum. The control parameter,  $a$ , was varied, corresponding to the amplitude of the driving force. The values of  $a$  for which phase portraits were plotted were 0.9, 1.07, 1.35, 1.47 and 1.5. By plotting data only every period of the driving force, a Poincare section was produced for the case of  $a = 1.5$

Finally, using a modified version of the above program, a bifurcation diagram was plotted of final periodic angles vs  $a$ .

## Results and Analysis

### Simple Pendulum

The trapezoidal rule was used to simulate the progress in time of a simple, undamped, non-driven pendulum. This was done twice, firstly using the linear approximation  $\sin(\theta) \approx \theta$ , and then for the non-linear case. This was done for various initial starting angles  $\theta$ . Phase-space diagrams were then plotted for each of these angles, with the linear case being plotted in green and the non-linear case plotted in red.

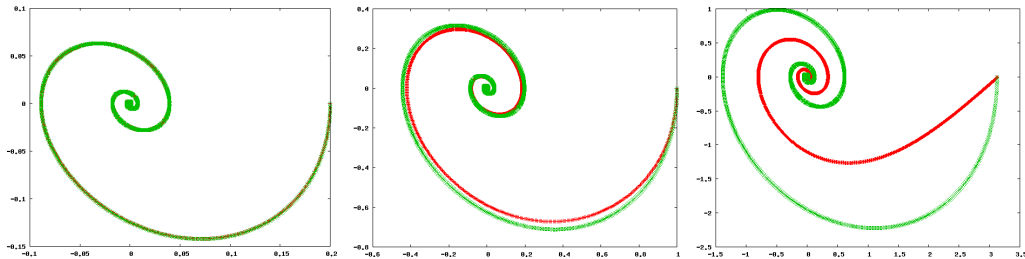


*Phase portraits for (l-r),  $\theta_i = 0.2$ ,  $\theta_i = 1$ ,  $\theta_i = 3.124$ , for both linear (green) and nonlinear (red)*

As we can see above, for small angle, the linear approximation is indeed a very good approximation. As the initial angle increases, we can see that the shape of the non-linear phase trajectory approaches that of the separatrix.

### Damped Pendulum

Using the Runge-Kutta method, the above steps were repeated for the case of a damped, undriven pendulum. The phase portraits are shown below.



*Damped phase portraits for (l-r),  $\theta_i = 0.2$ ,  $\theta_i = 1$ ,  $\theta_i = 3.124$ , for both linear (green) and nonlinear (red)*

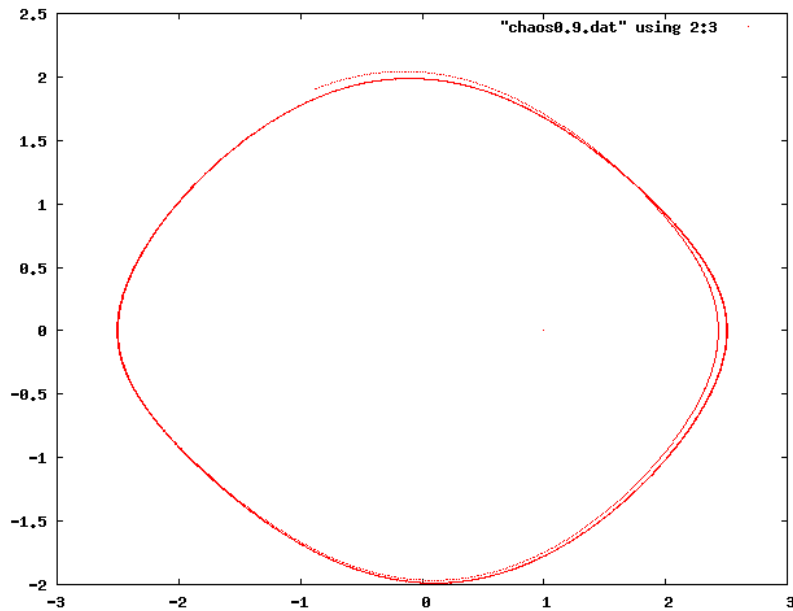
As we can see, for small starting angles, the linear case again agrees quite well for the non-linear case. For larger angles, we can see that even though initially the two equations yields quite different results, they eventually begin to agree after a sufficiently long time. This is even more evident in plots of angle vs time and angular velocity versus time, which are included in the appendix.

## Damped Driven Pendulum

Again using the Runge-Kutta method, phase portraits were obtained for damped driven pendula with various driving amplitudes. In each case, the following parameters were fixed:

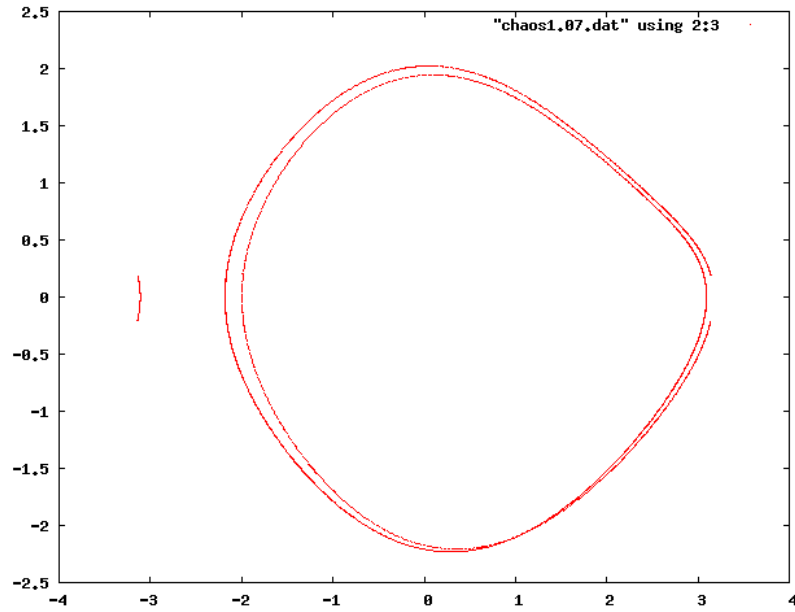
- $\theta_i = -2$
- $\omega_i = 0.5$
- $\beta = 0.5$

For  $a=0.9$ , we get normal pendulum behavior of a one-period closed phase trajectory. The tail at the top of the diagram shows a brief transition period before the motion settles into its periodic state.



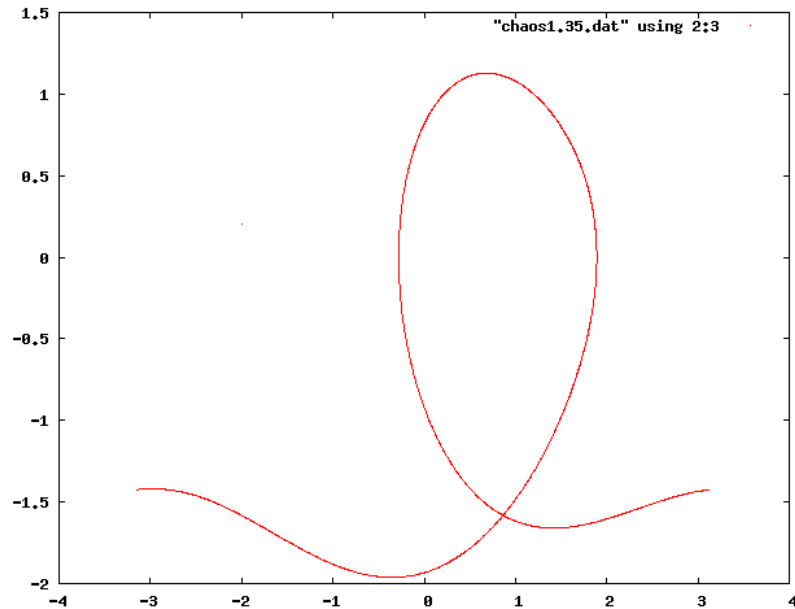
*Phase portrait for  $a = 0.9$*

For  $a=1.07$ , we can see that period doubling has occurred, as evident from the two distinct loops.



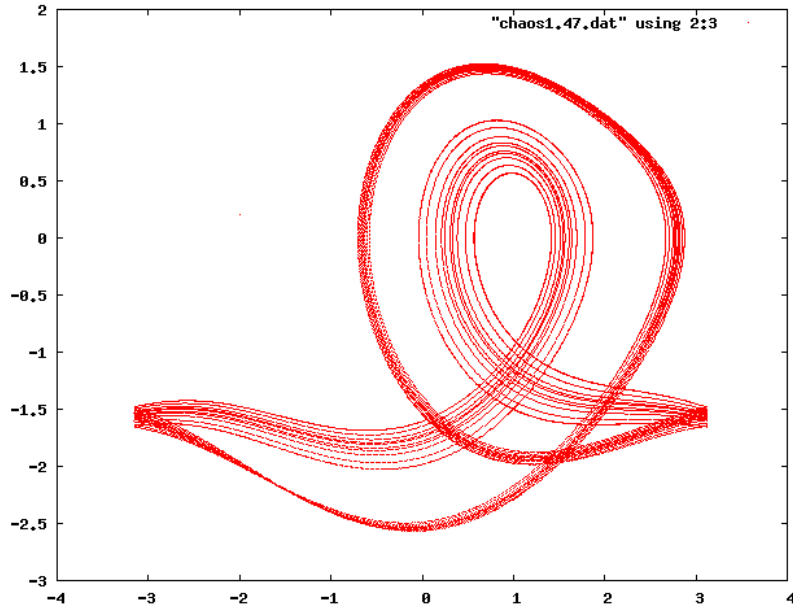
*Phase portrait for  $a = 1.07$*

For  $a=1.35$ , we begin to get more complicated motion, owing to rotations beginning to occur.



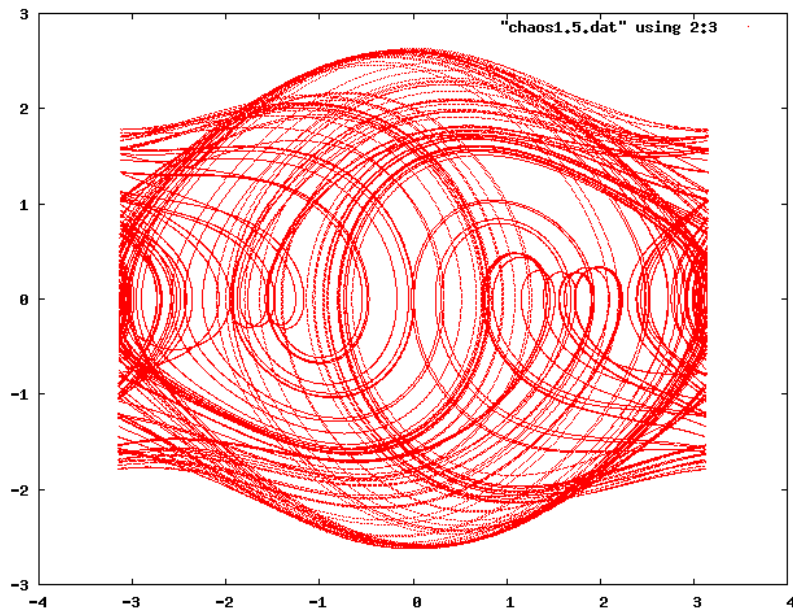
*Phase portrait for  $a = 1.35$*

For  $a=1.47$ , we see that period doubling has occurred multiple times, leading to a complicated phase trajectory whose period is approximately ten times that of the driving force.



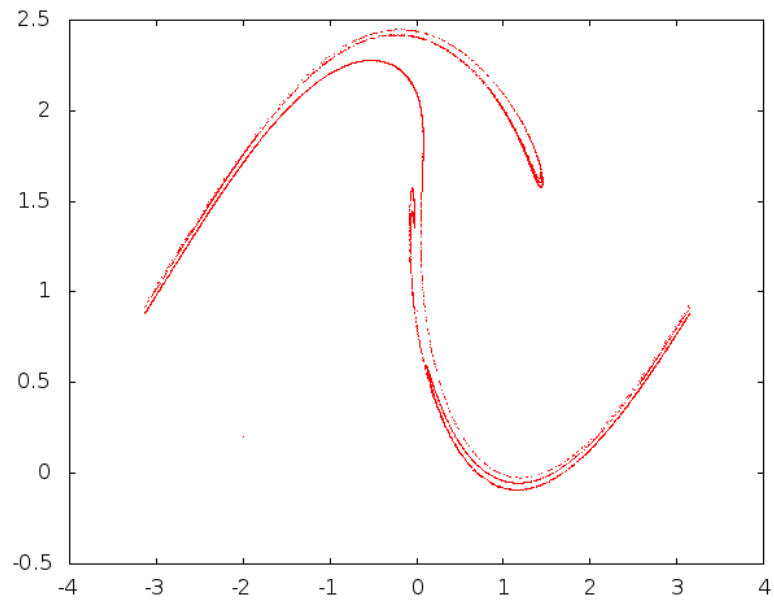
*Phase portrait for  $a = 1.47$*

For  $a=1.5$ , we see chaotic motion.



*Phase portrait for  $a = 1.5$*

One way of analysing this chaotic motion is by recording data once every period of the driving force, leading to the following Poincare Section:



*Poincare Section for  $a = 1.5$*

All of this information can be neatly summarised in the following bifurcation diagram:



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In this diagram, we can clearly see the features outlined above. Of particular interest:

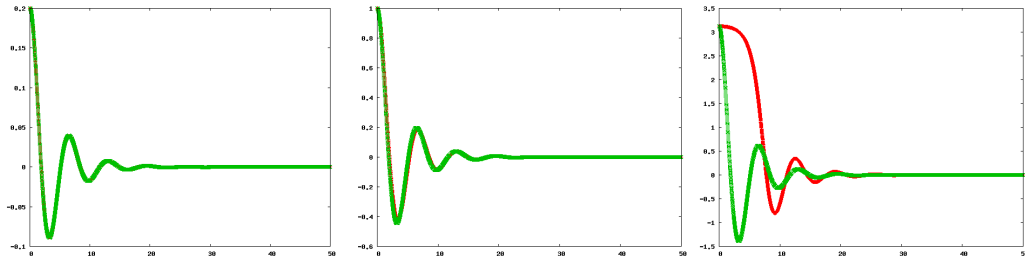
- At  $a=1.07$  we can see the period doubling occurring as the bifurcation diagram branches off into two parts.
- Between  $a=1.15$  and  $a=1.25$  we can see dramatic period doubling and potentially chaos occurring. Although this region was not investigated greatly in the lab, a phase diagram for  $a=1.2$  implied motion with an extremely long period. A phase diagram for  $a=1.26$  showed multiple-period motion with rotations. These diagrams are included in the appendix.
- After  $a=1.3$ , we again get single-period motion, this time for the case where the pendulum makes full rotations.
- At  $a=1.42$  we see period doubling starting again, ultimately leading to the chaotic region near  $a=1.5$

## Discussion and Conclusions

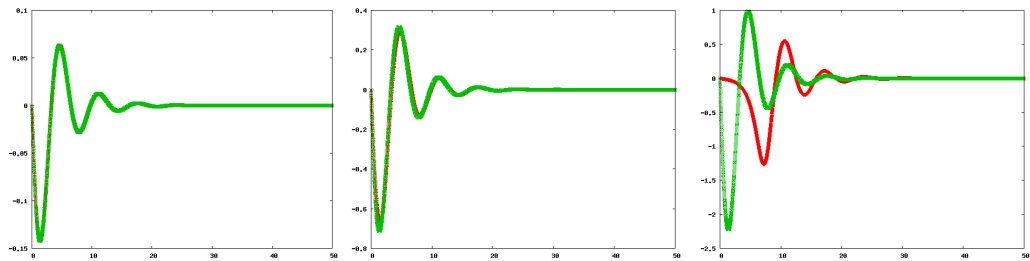
It was clearly seen that for large angles, the linear approximation of  $\sin(\theta) \approx \theta$  leads to large errors; this is the reason for most physical experiments on pendula requiring that all displacement angles be less than  $10^\circ$ . It was also seen that in the case of damped pendula, the linear and nonlinear cases tended to become close after a sufficient period of time had elapsed.

Using the Runge-Kutta method, the descent of a system into chaos through changes in a control parameter were clearly seen. Period doubling was also demonstrated. All of this information was neatly summarised in a bifurcation diagram.

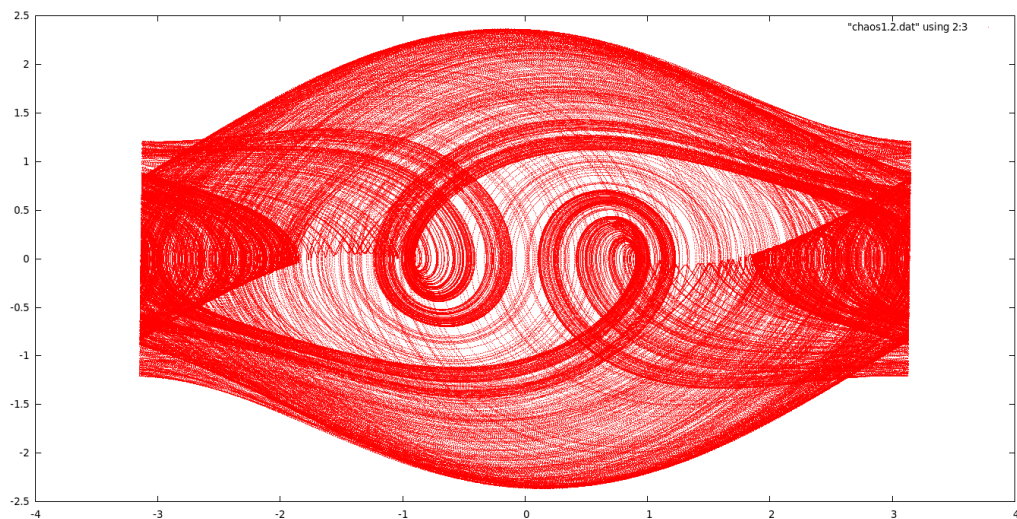
## Appendix of diagrams



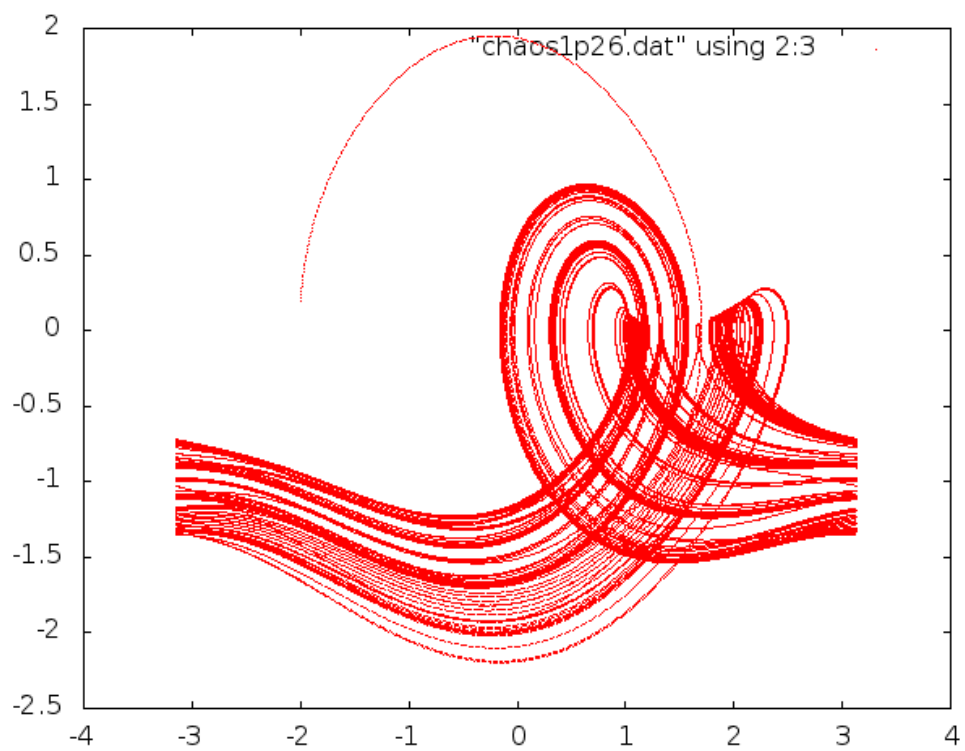
*Graphs of  $\theta$  vs time for (l-r),  $\theta_i = 0.2$ ,  $\theta_i = 1$ ,  $\theta_i = 3.124$ , for both linear (green) and nonlinear (red)*



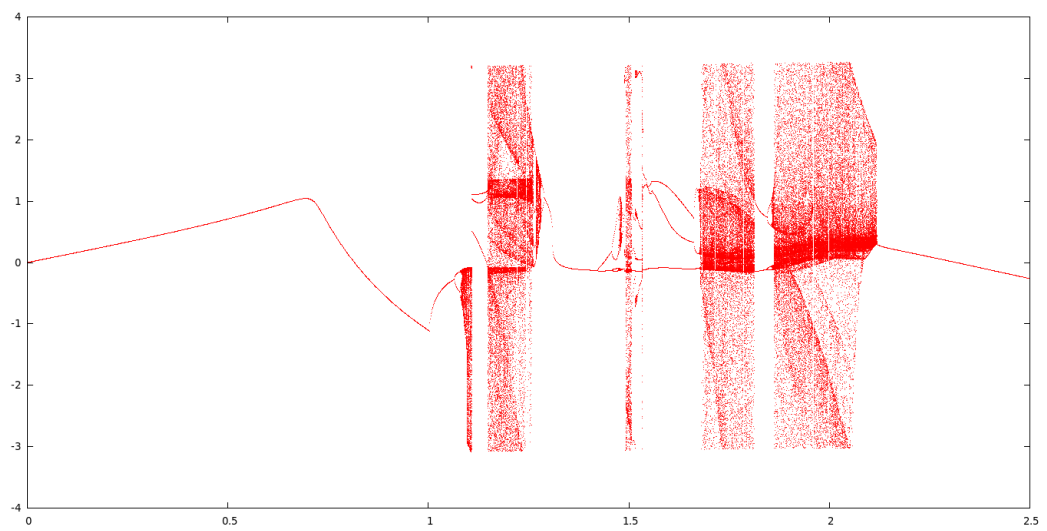
*Graphs of  $\omega$  vs time for (l-r),  $\theta_i = 0.2$ ,  $\theta_i = 1$ ,  $\theta_i = 3.124$ , for both linear (green) and nonlinear (red)*



*Phase portrait for  $a = 1.2$*



*Phase portrait for  $a = 1.26$*



*The bifurcation diagram, but this time with a wider range of  $a$ , from 0 to 2.5*