Classification of cylindrically symmetric static space-times according to their proper homothetic vector fields

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Abstract. A complete classification of cylindrically symmetric static spacetimes according to their proper homothetic vector field is given by using direct integration technique. Using the above mentioned technique we have shown that a very special class of the above space-times admit proper homothetic vector field. The dimensions of homothetic Lie algebras are 4, 5, 7 and 11.

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§1. Introduction

The aim of this paper is to study all the possibilities when the cylindrically symmetric static space-times admit proper homothetic vector fields by using direct integration techinque. Throughout M is representing the four dimensional, connected, hausdorff space-time manifold with Lorentz metric g of signature (-,+,+,+). The curvature tensor associated with g_{ab} , through Levi-Civita connection, is denoted in component form by $R^a{}_{bcd}$, and the Ricci tensor components are $R_{ab} = R^c{}_{acb}$. The usual covariant, partial and Lie derivatives are denoted by a semicolon, a comma and the symbol L, respectively. Round and square brackets denote the usual symmetrization and skew-symmetrization, respectively.

Any vector field X on M can be decomposed as

(1.1)
$$X_{a;b} = \frac{1}{2}h_{ab} + F_{ab}$$

where $h_{ab} = h_{ba}$ and $F_{ab} = -F_{ba}$ are symmetric and skew-symmetric tensor on M, respectively. If

$$h_{ab} = \alpha g_{ab}, \quad \alpha \in R$$

equivalent,

(1.2)
$$g_{ab,c}X^{c} + g_{bc}X^{c}_{,a} + g_{ac}X^{c}_{,b} = \alpha g_{ab}$$

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then X is called a homothetic vector field on M. If X is homothetic and $\alpha \neq 0$ then it is called proper homothetic while $\alpha = 0$ it is Killing [2, 3]. Further consequences and geometrical interpretations of (1.2) are explored in [1, 4]. It also follows from (1.2) that [1, 3]

$$L_X R^a{}_{bcd} = 0 L_X R_{ab} = 0.$$

The Lie algebra of a set of vector fields on a manifold is completely characterized by the structure constants C^a_{bc} given in term of the Lie brackets by

(1.3)
$$[X_b, X_c] = C_{bc}^a X_a, \quad C_{bc}^a = -C_{cb}^a,$$

where X_a are the generators. The Lie algebras for homothetic vector fields in term of structure constants are also given.

§2. Main results

Consider a cylindrically symmetric static space time in the usual coordinate system (labeled as (x^0, x^1, x^2, x^3)) with line element [7]

(2.4)
$$ds^{2} = -e^{v(r)}dt^{2} + dr^{2} + e^{u(r)}d\theta^{2} + e^{w(r)}d\phi^{2},$$

where v, u and w are some functions of r only. The linearly independent Killing vector fields are $[5, 6] \frac{\partial}{\partial t}, \frac{\partial}{\partial \theta}, \frac{\partial}{\partial \phi}$. A vector field X is said to be a homothetic vector field if it satisfies the equation (1.2). One can write (1.2) explicitly using (2.4) as

$$v'X^{1} + 2X_{.0}^{0} = 2c,$$

$$(2.6) X_0^1 - e^v X_1^0 = 0,$$

$$(2.7) e^u X_0^2 - e^v X_2^0 = 0,$$

$$(2.8) e^w X_{.0}^3 - e^v X_{.3}^0 = 0,$$

$$(2.9) X_{.1}^1 = c,$$

$$(2.10) e^u X_1^2 + X_2^1 = 0,$$

$$(2.11) e^w X_1^3 + X_3^1 = 0,$$

$$(2.12) u'X^{0} + 2X_{2}^{2} = 2c,$$

$$(2.13) e^w X_2^3 + e^u X_3^2 = 0,$$

$$(2.14) w'X^0 + 2X_3^3 = 2c.$$

Equations (2.6), (2.9), (2.10) and (2.11) give

(2.15)
$$X^{0} = A_{t}^{1}(t, \theta, \phi) \int e^{-v} dr + A^{2}(t, \theta, \phi) \\ X^{1} = cr + A^{1}(t, \theta, \phi) \\ X^{2} = A_{\theta}^{1}(t, \theta, \phi) \int e^{-u} dr + A^{3}(t, \theta, \phi) \\ X^{3} = A_{\phi}^{1}(t, \theta, \phi) \int e^{-w} dr + A^{4}(t, \theta, \phi)$$

where $A^1(t,\theta,\phi)$, $A^2(t,\theta,\phi)$, $A^3(t,\theta,\phi)$ and $A^4(t,\theta,\phi)$ are functions of integration. In order to determine $A^1(t,\theta,\phi)$, $A^2(t,\theta,\phi)$, $A^3(t,\theta,\phi)$ and $A^4(t,\theta,\phi)$ we need to integrate the remaining six equations. To avoid lengthy calculations here we will only present results for full details see [8].

Case (1) Four independent homothetic vector fields: In this case the space-time (2.4) takes the form

$$(2.16)$$

$$ds^{2} = -(cr + d_{9})^{2(1 - \frac{d_{5}}{c})}dt^{2} + dr^{2} + (cr + d_{9})^{2(1 - \frac{d_{10}}{c})}d\theta^{2} + (cr + d_{9})^{2(1 - \frac{d_{12}}{c})}d\phi^{2},$$

and homothetic vector fields in this case are

(2.17)
$$X^{0} = td_{5} + d_{6}$$

$$X^{1} = rc + d_{9}$$

$$X^{2} = \theta d_{10} + d_{11}$$

$$X^{3} = \phi d_{12} + d_{13}$$

where $d_5, d_6, d_9, d_{10}, d_{11}, d_{12}, d_{13} \in R$. The above space-time (2.16) admits four independent homothetic vector fields in which three are Killing vector fields which are given in (1.3) and one is proper homothetic vector field which is

$$(2.18) Y^1 = (0, r, 0, 0).$$

The generators in this case are:

$$X_1 = \frac{\partial}{\partial t}, X_2 = \frac{\partial}{\partial \theta}, X_3 = \frac{\partial}{\partial \phi} \text{ and } X_4 = r \frac{\partial}{\partial r}.$$

Here, all the structure constants are zero.

Case (2) Four independent homothetic vector fields: In this case the space-time (2.4) takes the form

$$(2.19) ds^2 = -(cr+d_9)^{2(1-\frac{d_5}{c})}dt^2 + dr^2 + d\theta^2 + (cr+d_9)^{2(1-\frac{d_{12}}{c})}d\phi^2.$$

Homothetic vector fields in this case are

(2.20)
$$X^{0} = td_{5} + d_{6}$$

$$X^{1} = rc + d_{9}$$

$$X^{2} = \theta c + d_{11}$$

$$X^{3} = \phi d_{12} + d_{13}$$

where $d_5, d_6, d_9, d_{11}, d_{12}, d_{13} \in R$. The above space-time (2.19) admits four independent homothetic vector fields in which three are Killing vector fields and one is proper homothetic vector field which is

$$(2.21) Y^2 = (0, r, \theta, 0).$$

The generators in this case are:

$$X_1 = \frac{\partial}{\partial t}, X_2 = \frac{\partial}{\partial \theta}, X_3 = \frac{\partial}{\partial \phi} \text{ and } X_4 = r \frac{\partial}{\partial r} + \theta \frac{\partial}{\partial \theta}.$$

The only non zero structure constant is: $C_{24}^2 = 1$

Case (3) Five independent homothetic vector fields:

In this case the space-time (2.4) takes the form

$$(2.22) ds^2 = (cr + d_9)^{2(1 - \frac{d_8}{c})} (-dt^2 + d\phi^2) + dr^2 + (cr + d_9)^{2(1 - \frac{d_{10}}{c})} d\theta^2$$

and homothetic vector fields in this case are

(2.23)
$$X^{0} = td_{8} + \phi d_{13} + d_{15} X^{1} = rc + d_{9} X^{2} = \theta d_{10} + d_{11} X^{3} = \phi d_{8} + td_{13} + d_{16}$$

where $d_8, d_9, d_{10}, d_{11}, d_{13}, d_{15}, d_{16} \in R$. The above space-time (2.22) admits five independent homothetic vector fields in which four are Killing vector fields and one is proper homothetic vector field which is

$$(2.24) Y^3 = (0, r, 0, 0).$$

The generators in this case are:

$$X_1 = \frac{\partial}{\partial t}, X_2 = \frac{\partial}{\partial \theta}, X_3 = \frac{\partial}{\partial \phi}, X_4 = t \frac{\partial}{\partial \phi} + \phi \frac{\partial}{\partial t} \text{ and } X_5 = r \frac{\partial}{\partial r}.$$

The only non zero structure constant are: $C_{14}^3 = C_{34}^1 = 1$.

Case (4) Five independent homothetic vector fields:

In this case the space-time (2.4) takes the form

(2.25)
$$ds^{2} = (cr + d_{9})^{2(1 - \frac{d_{8}}{c})} (-dt^{2} + d\phi^{2}) + dr^{2} + d\theta^{2}$$

and homothetic vector fields in this case are

(2.26)
$$X^{0} = td_{8} + \phi d_{13} + d_{14} X^{1} = rc + d_{9} X^{2} = \theta c + d_{17} X^{3} = \phi d_{8} + td_{13} + d_{10}$$

where $d_8, d_9, d_{10}, d_{13}, d_{14}, d_{17} \in R$. The above space-time (2.25) admits five independent homothetic vector fields in which four are Killing vector fields and one is proper homothetic vector field which is

$$(2.27) Y^4 = (0, r, \theta, 0).$$

The generators in this case are:

$$X_1 = \frac{\partial}{\partial t}, X_2 = \frac{\partial}{\partial \theta}, X_3 = \frac{\partial}{\partial \phi}, X_4 = t \frac{\partial}{\partial \phi} + \phi \frac{\partial}{\partial t} \text{ and } X_5 = r \frac{\partial}{\partial r} + \theta \frac{\partial}{\partial \theta}.$$

The only non zero structure constant are: $C_{14}^3 = C_{25}^2 = C_{34}^1 = 1$.

Case (5) Seven independent homothetic vector fields:

In this case the space-time (2.4) takes the form

(2.28)
$$ds^{2} = (cr + d_{7})^{2(1 - \frac{d_{6}}{c})} (-dt^{2} + d\phi^{2} + d\theta^{2}) + dr^{2}.$$

Homothetic vector fields in this case are

$$\left.\begin{array}{c}
X^{0} = td_{6} + \phi d_{11} + \theta d_{10} + d_{12} \\
X^{1} = rc + d_{7} \\
X^{2} = \theta d_{6} + td_{10} - \phi d_{13} + d_{15} \\
X^{3} = \phi d_{6} + td_{11} + \theta d_{13} + d_{14}
\end{array}\right\},$$

where $d_6, d_7, d_{10}, d_{11}, d_{12}, d_{13}, d_{14}, d_{15} \in R$. The above space-time (2.28) admits seven independent homothetic vector fields in which six are Killing vector fields and one is proper homothetic vector field which is

$$(2.30) Y5 = (0, r, 0, 0).$$

The generators in this case are:

$$X_1 = \frac{\partial}{\partial t}, X_2 = \frac{\partial}{\partial \theta}, X_3 = \frac{\partial}{\partial \phi}, X_4 = t\frac{\partial}{\partial \phi} + \phi\frac{\partial}{\partial t}, X_5 = t\frac{\partial}{\partial \theta} + \theta\frac{\partial}{\partial t}, X_6 = \theta\frac{\partial}{\partial \phi} - \phi\frac{\partial}{\partial \theta}$$

and

$$X_7 = r \frac{\partial}{\partial r}.$$

The only non zero structure constant are: $C_{14}^3 = C_{15}^2 = C_{25}^1 = C_{26}^3 = C_{34}^1 = C_{56}^4 = 1$ and $C_{36}^2 = C_{45}^6 = C_{46}^5 = -1$. Case (6) Eleven independent homothetic vector fields:

In this case the above space-time (2.4) becomes Minkowski space-time

(2.31)
$$ds^{2} = -dt^{2} + dr^{2} + d\theta^{2} + d\phi^{2}$$

homothetic vector fields in this case are

where $d_{10}, d_{11}, d_{12}, d_{13}, d_{14}, d_{15}, d_{16}, d_{17}, d_{18}, d_{19} \in R$. The above space-time (2.31) admits eleven independent homothetic vector fields in which ten are Killing vector fields and one is proper homothetic vector field which is

(2.33)
$$Y^6 = (t, r, \theta, \phi).$$

The generators in this case are:

$$X_{1} = \frac{\partial}{\partial t}, X_{2} = \frac{\partial}{\partial r}, X_{3} = \frac{\partial}{\partial \theta}, X_{4} = \frac{\partial}{\partial \phi}, X_{5} = t\frac{\partial}{\partial r} + r\frac{\partial}{\partial t},$$

$$X_{6} = t\frac{\partial}{\partial \phi} + \phi\frac{\partial}{\partial t}, X_{7} = \theta\frac{\partial}{\partial t} + t\frac{\partial}{\partial \theta}, X_{8} = \phi\frac{\partial}{\partial r} - r\frac{\partial}{\partial \phi}, X_{9} = \theta\frac{\partial}{\partial r} - r\frac{\partial}{\partial \theta},$$

$$X_{10} = \theta\frac{\partial}{\partial \phi} - \phi\frac{\partial}{\partial \theta} \text{ and } X_{11} = t\frac{\partial}{\partial t} + r\frac{\partial}{\partial r} + \theta\frac{\partial}{\partial \theta} + \phi\frac{\partial}{\partial \phi}.$$

The only non zero structure constant are: $C_{15}^1 = C_{16}^4 = C_{17}^3 = C_{11}^1 = C_{25}^1 = C_{21}^2 = C_{37}^1 = C_{39}^2 = C_{31}^4 = C_{31}^3 = C_{46}^1 = C_{48}^2 = C_{41}^4 = C_{68}^5 = C_{79}^5 = C_{71}^6 = C_{89}^1 = C_{91}^8 = 1$ and $C_{28}^4 = C_{29}^3 = C_{41}^3 = C_{56}^8 = C_{57}^9 = C_{58}^6 = C_{59}^7 = C_{67}^1 = C_{61}^7 = C_{81}^9 = -1$.

SUMMARY

In this paper a study of cylinderically symmetric static space-times according to their proper homothetic vector fields is given by using the direct integration technique. From the above study we obtain the following:

- (i) The space-times which admit four independent homothetic vector fields are given in equations (2.16) and (2.19) (see for details cases (1) and (2)).
- (ii) The space-times which admit five independent homothetic vector fields are given in equations (2.22) and (2.25) (see for details cases (3) and (4)).
- (iii) The space-time which admits seven independent homothetic vector fields are given in equation (2.28) (see for details case (5)).
- (iv) The space-time which admits eleven independent homothetic vector fields are given in equation (2.31) (see for details case (6)).

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